Abstract Submitted for the DFD14 Meeting of The American Physical Society

Floating element measurements of wall-shear stress exerted by high-Reynolds-number turbulent boundary layers WOUTIJN J. BAARS, University of Melbourne, KRISHNA M. TALLURU, University of Newcastle, NICK HUTCHINS, IVAN MARUSIC, University of Melbourne — Indirect methods to obtain the wall-shear stress τ_w , such as the Clauser chart fit, necessitate inherent assumptions of the boundary layer. Therefore, direct methods are preferred to measure τ_w and subsequently obtain the friction velocity $U_{\tau} = \sqrt{\tau_w/\rho}$. Floating elements are genuinely small to obtain local wall-shear stress measurements, but cope with low signal-to-noise ratios since the signal scales with the surface area ($\propto l^2$), where l is the characteristic length, and the error forces scale with hl; h represents the misalignment of the edges. Therefore, the capacious High Reynolds Number Boundary Layer Wind Tunnel at Melbourne incorporates a large floating element of $3m \times 1m$ over which the changes in boundary layer parameters are negligible, and hence, local measurements of U_{τ} are made with high accuracy. Smooth-wall results follow the $U_{\infty}/U_{\tau} = 1/\kappa \ln (\text{Re}_{\theta}) + C$ trend within $\pm 1\%$ ($\kappa = 0.380$ and C = 3.7) for typical test conditions ranging from $\text{Re}_{\theta} = 15,000$ to 45,000. Moreover, the device is used to measure U_{τ} corresponding to rough walls, and boundary layers that are perturbed by flush-mounted control devices within the element.

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Date submitted: 01 Aug 2014

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