

Abstract Submitted  
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**Some Divertor Scaling Considerations**<sup>1</sup> P.C. STANGEBY, University of Toronto — A case is advanced for “divertor non-scaling”, viz that absolute values of divertor density  $n_d \sim 10^{21} \text{ m}^{-3}$  and temperature  $T_d \sim 5 \text{ eV}$  need to be achieved for optimal demo/reactor-relevant studies. For  $T_d > 10 \text{ eV}$  sputtering is very strong; for  $T_d < 2 \text{ eV}$  there is risk of detachment and density limit. High  $n_d$  is required for high power, high duty cycle devices so that net erosion  $\ll$  gross erosion via prompt local re-deposition of sputtered material. This occurs when impurity neutral ionization mean free path  $\ll$  fuel ion gyro-radius (magnetic pre-sheath thickness); for  $B \sim 5 \text{ T}$  this requires  $n_d \gtrsim 10^{21} \text{ m}^{-3}$ . Thus peak parallel power flux density  $\sim 0.1 - 0.5 \text{ GW/m}^2$ . Modified two-point modeling then gives that: (a) “upstream” (e.g. outside midplane, separatrix), conditions,  $n_{eu}, T_u$ , are almost fixed, independent of R (device size) and  $P_{\text{SOL}}$  (power entering the SOL), and (b) the required  $P_{\text{SOL}} \sim R^1, R^{1.5}$  or  $R^2$ , depending on assumptions about target power width; the latter are discussed. A test device with these absolute  $n_d, T_d$  values will reproduce the most critical edge aspects of demo/reactors including power handling and material erosion/migration.

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